



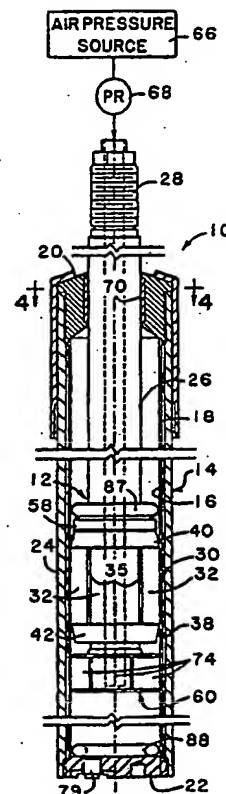
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(54) Title: FLUID ACTUATED FRICTION DAMPER

(57) Abstract

A fluid actuated friction damper having telescopically movable inner (12) and outer (14) bodies, the outer body (14) having an elongated, continuous friction surface (16). The inner body (12) includes a first set of friction shoes (32) engageable with the continuous friction surface, a fluid pressure responsive device for exerting a normal force to urge the friction shoes against the continuous friction surface (16), and a shuttle device (38) supporting the friction shoes (32) for limited axial movement between end stops on the inner body. The inner body also provides fluid pressure communication between an external source (66) of pressurized fluid and the fluid pressure responsive device when the shuttle (38) is at one of the stops and for isolating the fluid pressure responsive device from the external source when the shuttle is moved from the one stop. A second set of friction shoes (74) and a second fluid pressure responsive device for exerting a normal force to urge the second shoes (74) against said continuous friction surface (16) independently of the first set of friction shoes (32). The pressure responsive devices for both friction shoe sets are controlled by regulating the pressure of fluid supplied to the inner body from the external fluid pressure source (66). The normal force for both sets of friction shoes may be developed by a single externally controlled fluid pressure (68) or, alternatively, by separate externally controlled fluid pressures.



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FLUID ACTUATED FRICTION DAMPERBACKGROUND OF THE INVENTION

This invention relates to shock absorbers, and, more particularly, to fluid actuated friction dampers. The friction dampers of the present invention are useful for a wide range of friction damping applications but are intended principally for use in land vehicle suspension systems.

In U.S. Patent No. 4,979,575, issued to the present inventor on December 25, 1990, embodiments of a fluid actuated friction damper are disclosed in which relative movement between inner and outer telescopic bodies is damped by friction shoes on the inner body expanded by fluid pressure into engagement with a continuous internal surface on the outer body. In certain of the disclosed friction damper embodiments, an external dual pressure source is used to expand a single set of friction shoes under one pressure during one direction of relative inner and outer body movement and under a different pressure in the other direction of such relative movement. In other embodiments disclosed, a single external pressure source is applied alternately to axially spaced sets of friction shoes of differing effective area. Thus, in one direction of relative inner and outer body movement, the single fluid pressure is applied to one of the two sets of friction shoes whereas in the other direction of such relative movement, the same pressure is applied to the other of the two sets of shoes.

From the different embodiments disclosed in the prior patent, it is apparent that in one case, the friction force is changed upon directional reversal of body movement, while in the other case, the effective friction area is changed on directional reversal. In both cases, the relative direction of inner and outer body movement must be sensed, a controller is required to respond to the sensed direction of relative movement, and either the pressure of the fluid is required to be changed, as in the case of a dual pressure source, or the fluid flow path between the external source of fluid pressure is required to be changed, with each sensed direction of body movement reversal.

While the operational principles of the friction damper embodiments disclosed in the aforementioned patent are sound, the external pressurized fluid system is relatively complicated, and as such, costly from the standpoints of manufacture, installation and maintenance. As a result, the benefits of the controlled fluid pressure actuated friction damper represented by the embodiments disclosed in the prior patent have not been realized in a commercially competitive shock absorber market.

10 SUMMARY OF THE INVENTION

Disclosed herein is a fluid actuated friction damper comprising:

telescopically movable inner and outer bodies;
the outer body having an elongated, continuous
15 friction surface;

the inner body comprising friction shoe means engageable with said continuous friction surface, fluid pressure responsive means for exerting a normal force to urge said friction shoe means against said continuous friction
20 surface, a shuttle device supporting said friction shoe means for limited axial movement between end stops on said inner body, and means for establishing fluid pressure communication between an external source of pressurized fluid and said fluid pressure responsive means when said shuttle device is at one
25 of said stops and for isolating said fluid pressure responsive means from said external source when said shuttle device is moved from said one stop.

In accordance with the present invention, the problems associated with the relatively complex control
30 systems required for the friction dampers of the type disclosed in the aforementioned patent are substantially avoided by a pressurized fluid actuated friction damper in which a regulated external source of fluid pressure is maintained in communication with one or more internal pressure
35 chambers ported selectively by a friction shoe member which is moveable directly in response to directional reversals of the relatively moveable inner and outer bodies.

Additional features and advantages of the invention will be set forth in part in the description which follows,

and in part will be obvious from the description, or may be learned by practice of the invention. The advantages of the invention will be attained by means of the elements and combinations particularly pointed out in the appended claims.

5 In accordance with the purpose of the invention, as embodied and broadly described herein, the fluid actuated friction damper of the invention comprises telescopically movable inner and outer bodies, the outer body having an elongated, continuous friction surface. The inner body
10 includes friction shoe means engageable with the continuous friction surface, fluid pressure responsive means for exerting a normal force to urge the friction shoe means against the continuous friction surface, and a shuttle device supporting the friction shoe means for limited axial movement between end
15 stops on the inner body. The inner body also provides fluid pressure communication between an external source of pressurized fluid and the fluid pressure responsive means when the shuttle means is at one of the stops and for isolating the fluid pressure responsive means from the external source when
20 the shuttle means is moved from the one stop.

In another aspect of the invention, the fluid actuated friction damper includes a second friction shoe means and a second fluid pressure responsive means for exerting a normal force to urge the second shoe means against said
25 continuous friction surface independently of the first mentioned friction shoe means. The pressure responsive means for both friction shoe means are controlled by regulating the pressure of fluid supplied to the inner body from the external fluid pressure source. Further, the normal force for both
30 friction shoes may be developed by a single externally controlled fluid pressure or, alternatively, by separate externally controlled fluid pressures.

In still another aspect of the invention, the outer body is formed of inner and outer cylindrical walls connected
35 at opposite ends and separated from each other between the opposite ends by an annular space. The annular space forms part of a fluid passageway by which separated chambers, defined by opposite ends of the inner body, the inner cylindrical wall and the opposite ends of the outer body, are

connected for venting air between the separated chambers upon relative movement of said inner and outer bodies to inversely vary the volume of such chambers, respectively.

It is to be understood that both the foregoing
5 general description and the following detailed description are exemplary and explanatory only and are not restrictive of the invention as claimed.

BRIEF DESCRIPTION OF THE DRAWINGS

The accompanying drawings, which are incorporated
10 in and constitute a part of this specification, illustrate embodiments of the invention and together with the description, serve to explain the principles of the invention. In the drawings,

Fig. 1 is a fragmented partial longitudinal cross-
15 section depicting an embodiment of the present invention;

Fig. 2 is an enlarged complete longitudinal cross-
section of a central portion of the embodiment illustrated in Fig. 1;

Fig. 3 is a cross-section on line 3-3 of Fig. 2;
20 Fig. 4 is an enlarged cross-section on line 4-4 of Fig. 1;

Fig. 5 is a cross-section on line 5-5 of Fig. 2;

Fig. 6 is a cross-section on line 6-6 of Fig. 2;

Fig. 7 is a largely schematic view illustrating an
25 alternative embodiment of the present invention;

Fig. 8 is a fragmented longitudinal cross-section illustrating a variation applicable to both illustrated embodiments of the invention;

Fig. 9 is an enlarged fragment of the cross-section
30 in Fig. 8;

Fig. 10 is a cross-section on line 10-10 of Fig. 9;

Figs. 11 through 13 are perspective views of various modifications of an elastomeric tube of this invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

35 Reference will now be made in detail to the present preferred embodiments of the invention, examples of which are illustrated in the accompanying drawings. Wherever possible, the same reference numbers will be used throughout the drawings to refer to the same or like parts.

In accordance with the present invention, a fluid actuated friction damper is provided with inner and outer bodies arranged for telescopic movement relative to each other. In practice, the respective inner and outer bodies are connected to relatively moveable member between which movement is to be inhibited or damped. In automotive vehicle suspension systems, such relative movement is termed "jounce" when the relatively movable members move toward one another and "rebound" when the members move away from each other. These terms shall be used herein and in the appended claims irrespective of the specific application for which the invention is used.

At least one friction shoe is supported for limited axial movement on the inner body by a shuttle device associated with valving ports for opening and closing fluid communication between a regulated external pressure source and an internal pressure chamber by which the at least one friction shoe is forced into engagement with a continuous inwardly facing friction surface on the outer body. Movement of the shuttle on the inner body is responsive to the relative direction of inner and outer body movement. Preferably, shuttle movement opens communication between the external pressure source and the appropriate internal pressure chamber in response to rebound and closes off such communication in response to jounce.

In Figs. 1-6, an exemplary embodiment of a fluid actuated friction damper incorporating the present invention is generally designated by the reference numeral 10 and shown to include an inner body 12 and an outer body 14 having a cylindrical inwardly facing friction surface 16. The surface 16 is formed on the interior of a thin walled cylindrical tube 18 supported at one end by an annular collar 20 and at the opposite end by an end wall 22. The collar 20 and end wall 22 are secured structurally by an outer body cylindrical wall 24. As illustrated, the inner wall 18 is spaced slightly from the outer wall 24 both to insulate the inner wall 18, particularly the inner surface 16 thereof, from physical deformation by external forces exerted on the outer wall 24 and also to provide an air passage for heat dissipation and

cooling. In applications where the outer wall 24 is not subject to deformation by external forces, such as laterally induced tube collapsing forces or thermal distortion caused by welding, for example, the inner wall 18 may be eliminated and the surface 16 may be provided directly on the inside of the outer wall 24.

The inner body 12 includes an elongated hollow rod 26 extending through the collar 20 to an exterior threaded end 28 and supporting a friction shoe assembly 30 at its opposite or inner end. The threaded end 28 of the rod 26, in use, is fitted to one of the two members (not shown) between which movement is to be damped. The outer body 14 is connected to the other of such two members by an appropriate fitting (also not shown).

The friction shoe assembly 30 in the illustrated embodiment, as shown most clearly in Figs. 1-3, includes four arcuately convex friction shoes 32 positioned radially outside of an expansible elastomeric tube 34 by arcuate shims 32a to which the respective shoes are connected or with which the respective shoes are integrally formed. Each of the shims 32a has an arcuate width greater than the corresponding dimension of each shoe 32. As a result, the shoes are always spaced from each other by gaps 35 and the inwardmost position of the shoes is determined by edge-to-edge engagement of the shims 32. The interior of the tube 34 defines part of an internal pressure chamber 36 by which the friction shoes 32 are forced outwardly into engagement with the friction surface 16 of the outer body 14.

As shown in Fig. 2, in the illustrated friction damper embodiment 10, the shuttle device is designated generally by the reference numeral 38 and includes end rings 40 and 42 secured, such as by press fit, for example, to opposite ends of a cylindrical sleeve 44 dimensioned to be freely slidable on the outside of the hollow rod 26. Each of the end rings 40 and 42 is of a dish-shaped configuration to establish an exterior end abutment surface 46, an annular tube support surface 47, and an outwardly flared axial wall 48 terminating in a radial surface 50. The axial walls 48 of the end rings 40 and 42 extend toward each other to confine the

ends of the elastomeric tube 34. The mutually facing annular support surfaces 47 on the end rings 40 and 42 are spaced to provide a compressive bias at the ends of the tubular wall 34 to cause the tube to bulge outward with no application of fluid presence on the inside thereof. Also, the radial surfaces 50 of the end rings, being of fixed axial spacing by connection to the ends of the sleeve 44, serve to fix the axial position of the friction shoes 32 in the shuttle 38.

The shuttle sleeve 44 is formed with a plurality of radial ports 52 which open outwardly to the pressure chamber 36 on the inside of the elastomeric tube 34. The hollow rod 26 is similarly provided with radial ports 54 which are interconnected by a peripheral manifold groove 56 on the exterior of the hollow rod 26.

The shuttle 38 is positioned on the hollow rod 26 between a first stop defined by a collar 58 threaded to the rod at a location spaced from the end of the rod 26 and a second stop defined by an end fitting 60 fixed to the inner end of the rod 26. Preferably, the second stop is established by an annular rail 61 on the fitting 60. In this way, the second stop may be precisely formed by machining the rail and so that when the surface 46 on the shuttle 38 abuts the rail, the ports 52 and 54 are precisely aligned. Also the ports 54 and the manifold groove 56 are positioned on the hollow rod 26 between spaced O-rings 62 and 64 which make a sliding seal with the inside of the shuttle sleeve 44. In addition to being freely slidable on the rod 26, the shuttle sleeve 44 is sufficiently loose on the rod 26 to permit venting of air between the inside of the shuttle sleeve 44 and the outside of the rod 26. In the axial space between the O-rings 62 and 64, however, passage of pressurized fluid between the inside of the shuttle sleeve 44 and the outside of the rod 26 is confined. Thus, movement of the shuttle 38 between a position in which the shuttle ports 52 are located beyond or outside of the space between the O-rings 62 and 64, that is, the position illustrated in Fig. 2, and a position in which the shuttle ports 52 are located between the O-rings, will close and open, respectively, fluid communications between the interior of the hollow rod 26 and the chamber 36 at the inside

of the pressure responsive elastomeric tube 34.

As shown in Fig. 1, an external pressure source 66, represented schematically, is connected through a pressure regulator 68 to the interior of the hollow rod 26. While the
5 amount of air pressure to which the interior of the hollow rod 26 is subjected is preferably variable, the pressure source is in communication with the interior of the hollow rod 26 at all times during operation of the friction damper 10.

In accordance with the present invention, the inner
10 and outer bodies are guided by an arrangement of bearings to ensure alignment of the bodies independent of fluid actuated friction components. Also, the bearings and friction components of the invention are constructed so that fluid pressure controlled friction damping is maximized as against
15 uncontrolled parasitic friction and the unwanted effects of fluid compression or expansion resulting from relative movement of the inner and outer bodies.

In the illustrated embodiment and with particular reference to Figs. 1 and 4 of the drawings, the hollow rod 26
20 of the inner body 12 is constrained to alignment with the collar 20 at one end of the outer body 14 by a slide bearing 70 at the inner surface of the collar 20. The bearing 70 is formed by four segments 71 of low friction material to be described in more detail below; however, it is contemplated
25 that one or more such segments may be used in the bearing to provide symmetry of slide bearing support about the circumference of the hollow rod 26. It is to be noted that the segments 71 are spaced by radial gaps 72. The gaps 72 provide venting passageways by which air within the outer body
30 14 between the inner end of the inner body 12 and the collar 20 may be vented to atmosphere. Similarly, the gaps 35 between the shuttle carried friction shoes 32 provide venting passageways between the friction shoe assembly 30 and the inner friction surface 16 of the outer body 14. Also, and as
35 shown in Figs. 2, 5, and 6, the end fitting 60 is formed with axial vent ports 73 to avoid any compression of air caused by relative movement of the shuttle toward the end fitting. The ports 73 are additionally sized and oriented to function as spanner engagement holes by which the end fitting 60 may be

threaded onto the hollow rod 26.

In the illustrated embodiment, the venting gaps 35 and 72 are provided by the use of multiple, circumferentially spaced shoes. However, a single, axially split, cylindrical shoe could be used. In the case of such a cylindrical friction shoe or guide bearing, spaced axial grooves may be cut or otherwise formed in the sliding surface thereof.

A further guide bearing arrangement is provided on the fitting 60 at the inner end of the hollow rod 26. As may be understood by reference to Figs. 2, 5, and 6 of the drawings, the outer periphery of the fitting 60 is recessed to receive a plurality of outwardly convex arcuate segments 74. Inwardly of the peripheral recess in which the segments 74 are received, the fitting 60 is provided with an undercut formation 76 in a manner such that the opposite axial ends of the segments 74 bear directly against the body of the fitting 60. As a result, the axial ends of the segments are confined between the fitting 60 and the inner surface 16 of the outer wall to provide bearing support between the inner end of the rod and the outer body 14. As may be seen in Figs. 5 and 6, four segments 74 are employed in the illustrated embodiment, the segments being spaced by gaps 78 again for the purpose of permitting air to be vented across the fitting 60 in the outer body 14 as the inner body moves axially in the outer body. As indicated above with respect to the bearing 70, the use of four segments provides symmetry of bearing support at the end of the inner body 12 about the circumference of the fitting 60. However, it is contemplated that other symmetrical arrangements, such as one or more such segments, may provide the equivalent bearing support.

A further venting provision is provided at the closed end of the outer body. In the illustrated embodiment and as shown in Fig. 1, a filtered vent plug 79 is mounted in the end wall 22. Thus, any tendency for air to compress by jounce movement of the inner body 12 toward the closed end of the outer body will be avoided by venting air through the vent plug 79. Similarly, any reduction of air pressure on rebound movement of the inner body away from the closed end 22 will be minimized by air passing inwardly through the vent plug 79.

In accordance with the present invention, a controlled pressure actuated friction force may be exerted at all times between the inner and outer bodies. Such controlled friction force will be applied between the bodies during both
5 jounce and rebound relative movement between the two bodies.

In the illustrated embodiment, the controlled fluid pressure actuated friction force is applied to the arcuate segments 74 which define the bearing support for the inner end of the hollow rod 26. In particular, the under cut portion
10 76 of the fitting receives an elastomeric tubular member 80 having properties similar, if not identical, to the properties of the elastomeric tube 34 described above with reference to the friction shoe assembly 30. Outwardly of the elastomeric tube 80, a plurality of arcuately convex shims 82 are
15 positioned so as to lie between the outside of the elastomeric tube 80 and inside of the bearing shoe segments 74. Inside the elastomeric tube 80, the under cut formation 76 defines an internal pressure chamber to which compressed air from the external source 66 is supplied by way of the hollow rod 26
20 through radial ports 84. A sealed drain plug 87 is threaded into the bottom of the end fitting 60 to facilitate draining of any liquid condensate which may accumulate in the hollow rod 26.

In light of the construction of the end fitting 60
25 as thus shown and described, the axial central region of the bearing segments 74 function as fluid actuated friction shoes forced by fluid pressure against the inside surface 16 of the outer body 14. At the axial ends of the bearing segments 74, the guiding function of the segments is preserved because the
30 direct bearing of the ends of the segments against the end fitting is independent of fluid pressure.

In accordance with the invention, provision is made for cushioning the end limits of moving component travel. As shown in Fig. 2, O-rings 85 and 86 are supported adjacent the
35 mutually facing stop surfaces of the collar 58 and the end fitting 60 in the illustrated embodiment. The O-rings 85 and 86 are retained by relatively shallow circumferential grooves in the hollow rod 26 so as to project into the path of the ends of the shuttle 38. Thus, as the shuttle moves between

the end stops defined by the collar 58 and the end fitting 60, it is cushioned at the end of such relative travel by the O-rings 85 and 86.

In addition, relative travel between the inner body and the outer body between the maximum physical limits of travel is similarly cushioned. In the illustrated embodiment, a relatively large elastomeric O-ring 87 is supported on the hollow rod 26 between the friction shoe assembly 30 and the interior of the end collar 20. A similar O-ring 88 is positioned between the end fitting 60 on the inner body 12 and the end wall 22 on the outer body. Thus, in the event that the bodies move through maximum permitted travel, the large elastomeric O-rings 87 and 88 will cushion the engagement of components with each other.

In accordance with the present invention, the material of all nonmetallic friction members, for example, the segments 71 of the collar bearing 70, the shuttle carried friction shoes 32, and the bearing/friction shoe segments 74 on the end fitting 60, in the illustrated embodiment, is preferably selected to develop interfacial friction by composite/counterface interface with the metal surfaces in which they are in contact. Examples of such materials are polytetrafluoroethylene (PTFE) filled polyphenylene sulfide (PPS), or composite ultra high molecular weight polyethylene. Such materials exhibit very low coefficients of friction as a result of wear debris from the PTFE, for example, forming a very effective lubricant as an interface between the friction shoes or guide segments and the metal surfaces with which they are in contact. Also, unlike conventional Coulombic friction interfaces, the static coefficient of friction of composite/counterface interfaces, in accordance with the present invention, is lower than the dynamic coefficient of friction. As a result, the "stick/slip" behavior of conventional friction materials is avoided.

Although the friction damper of the present invention is useful in a wide range of motion damping applications, it is principally intended for use in land vehicle suspension systems. In an automotive application, for example, the damping device might be used as a suspension

strut or as a shock absorber. In this application, a single friction device 10 is mounted between the chassis and each wheel of the vehicle by connecting the threaded end 28 on the hollow rod 26 to the chassis and connection of the outer body 14 to a wheel supporting axle or equivalent. The external pressure source 66, manifested in practice by an air compressor and pressure storage tank, for example, is supported on the chassis and connected by conduits to the hollow rods of each friction damper device 10. A single pressure regulator ensures that the magnitude of fluid pressure supplied to all friction damper devices 10 will be the same. Through use of appropriate conduit connections, the pressure regulator 68 may be located in a position convenient to the operator of the automotive vehicle. In more sophisticated suspension systems, such as "active systems," for example, a separate pressure regulator may be provided for each device.

During operation, travel of the automotive vehicle will cause the inner and outer bodies 12 and 14 of the respective shock absorber devices 10 to move relative to each other in jounce and rebound directions of movement. The shuttle 38 on the inner body of each device will move between the stop collar 58 and the fitting 60 in correspondence with such inner and outer body movement.

In Fig. 2, the shuttle 38 is illustrated at its upward limit of travel, that is, with the abutment surface 46 of the end ring 40 engaged in abutment with the inner stop collar 58. In this position, the ports 52 are isolated by the O-ring 62 from the ports 54 and the manifold groove 56 so that fluid communication between the interior of the hollow sleeve 26 and the pressure chamber 36 inside the elastomeric sleeve 34 is closed. The illustrated position of the shuttle 38 in Fig 2 is, moreover, the position the shuttle would take during relative jounce movement between the inner and outer bodies 12 and 14. As a result, during jounce movement, the friction shoes 32 are not forced by fluid pressure against the friction surface 16 of the outer body 14. However, controlled friction damping of inner and outer body movement in jounce will occur due to communication between the regulated external source of

fluid pressure and the internal pressure chamber defined by the under cut portion 76 in the end fitting 60. In particular, such fluid pressure acting against the interior of the elastomeric tube 80 through the open ports 84 will exert a controlled force to urge the central portions of the bearing segments 74 into frictional engagement with the surface 16 of the outer body 14.

When the inner and outer bodies 12 and 14 move in the opposite direction, or in rebound, the shoes 32 maintain a sufficient drag on the surface 16 so that the shuttle 38 will move until the abutment surfaces 46 on the end ring 42 engage the upper surface of the end fitting 60. The drag adequate to insure such shuttle movement may be adjusted by varying the amount of end bias on the elastomeric tube 34 by the end rings 40 and 42, thus determining the amount of outward force exerted by outward bulging of the tube 34 with no internal pressure. In this position, the ports 52 on the shuttle sleeve 44 will be aligned with the manifold groove 56 at the exterior of the hollow rod ports 54 so that pressure inside the hollow rod 26 will be communicated with the internal pressure chamber 36 defined by the elastomeric tube 34. Thus, in rebound movement of the inner and outer bodies, the friction shoes 32 will be forced by a fluid pressure outwardly against the inner surface 16 of the outer body 14 in a manner to supplement the controlled frictional drag of the end fitting carried bearing segments 74 biased by the same fluid pressure in the described embodiment.

Because of the low coefficient of friction in the nonmetallic members 71, 32 and 74, the guiding function of the collar bearing 70 and of the end portions of the shoe segments 74 in the illustrated embodiment, will have little or no parasitic frictional damping effect on relative movement of the inner and outer bodies 12 and 14. On the other hand, a combination of friction surface area and normal force is available to control the frictional drag exerted between the inner and outer bodies. For example, the shuttle carried friction shoes 32 in the illustrated embodiment are shown to have much larger surface area than the surface area of the shoes 74 or portion thereof subject to variable normal force

by regulated fluid pressure. As a result, the frictional drag for a given normal force is significantly greater in rebound than it is in jounce movement of the inner and outer bodies. It is contemplated, therefore, that the respective surface area sizes of the shoes 74 may be selected to provide only a slight added friction drag in rebound as compared to jounce, given the general construction of the illustrated friction damping embodiment 10.

In Fig. 7, an alternative embodiment of the present invention is shown to be incorporated in a friction damper, generally designated by the reference numeral 90, and in which parts previously described are identified by identical reference numerals. In the embodiment of Fig. 7, a multi-port fitting 91 is connected between the air pressure source 66 and the interior of the hollow rod 26. Fluid pressure is supplied by the regulator 68 through a port 92 of the fitting 91, directly to the interior of the hollow rod 26. Communication of fluid pressure between the regulator 68 and the friction shoe assembly 30, through the port 92, is the same as the embodiment described with reference to Figs. 1-6. In the friction damper 90 of Fig. 7, however, a closed pipe 93 extends from a separate port 94 in the fitting 91 to a plug 95 located above the ports 84 which open to the internal chamber positioned behind the pressure responsive elastomeric member 80 in the end fitting 60. The plug 95 thus closes off or isolates the pressure responsive member 80, by which the central portions of the shoe segments 74 on the end fitting 60 are forced into engagement with the friction surface 16, from fluid pressure originating at the regulator 68. A separate pressure regulator 96 is provided between the air pressure source 66 and the conduit 90.

As a result of the modification shown in Fig. 7, the frictional drag applied between the bearing shoe segments 74 and the continuous friction surface 16 on the outer body 14, at all times during both jounce and rebound movement, may be regulated independently of the fluid pressure used to operate the friction shoe assembly 30 during rebound movement only. Thus, the measure of control over the operating characteristics of the friction damper 90 is increased over

that available with the friction damper 10 described above with reference to Figs. 1-6. In both embodiments, however, highly effective, controlled friction damping operation is provided by a relatively simple damper construction, which is
5 inexpensively manufactured and installed, and which is capable of low maintenance operation.

In accordance with a further feature of the present invention, the annular space separating the inner and outer cylindrical walls of the outer body forms part of a fluid
10 passageway for venting air between separated chambers in the outer body at opposite ends of the inner body. As the volumes of those chambers vary inversely upon relative movement of the inner and outer bodies, the venting of air between the chambers serves to maintain pressure in equilibrium.
15 Additionally, the annular space may be vented to the atmosphere for cooling purposes.

In Figs. 8-10, a variant of the friction damper embodiment described with reference to Fig. 1 is designated generally by the reference numeral 10'. Parts previously
20 identified with reference to Fig. 1 are designated by the same reference numerals.

As previously described, the outer body 14 of the friction damper 10' is defined by inner and outer cylindrical walls 18 and 24, respectively, separated by an annular space
25 100. The annular space extends for the length of the device 10 between the connections of the inner and outer walls at one end by the end wall 22, and at the other end by the annular collar 20. In the friction damper variant 10', radial ports 102, specifically four such ports, extend through the inner
30 cylindrical wall 18 near opposite ends thereof. As a result, as the inner body 12 is moved relative to the outer body 14, the chambers defined at opposite ends of the inner body with the outer body will vary in volume. To avoid the effects of fluid pressure on the relative movement between the inner and
35 outer bodies, the passageway provided by the ports 102 and the annular space 100 vents air between the chambers to equalize fluid pressure irrespective of volume changes in the two chambers.

Additionally, and as shown most clearly in Fig. 9

of the drawings, the annular chamber 100 is vented to the atmosphere. In this respect, the upper end of the fluid actuated friction damper, both as illustrated in Fig. 8 and in the previously describe embodiments, is provided with an exterior end bell 104 having an inwardly inclined annular flange portion 106 at its upper end in firm engagement with the annular collar 20. The end bell 104 further includes a depending cylindrical skirt portion 108 which is spaced outwardly from the outer wall 24 of the outer body 14 by an annular clearance gap 112.

In the variant of Figs. 8-10, the annular collar is provided with venting slots 110 so that the passageway defined by the annular clearance 112 between the end bell 104 and the outer wall 24 is opened to the atmosphere. Radial ports 114 are formed in the outer wall near the end thereof, connected by the annular collar 20. Thus, the annular space 100 between the inner wall 18 and the outer wall 24 of the outer body 14 is vented to the atmosphere along the annulus 112 and slots 110 in the collar 20. As a result of this construction, heat developed by friction between the inner body 12 and the friction surface 16 may be dissipated by air circulating outwardly through the ports 114, annulus 112 and slots 110.

Figures 11 through 13 show modifications of the elastomeric tube 34 discussed in particular with respect to Figure 3. In Figures 11 through 13, elastomeric tube 34 carries on its outside surface rings 34a as seen in Figures 11 and 12, or strips 34a as seen in Figure 13. These rings or strips 34a, two or more being desirable but not a limitation, are preferably comprised of an elastomeric material and may be separately or integrally formed with elastomeric tube 34. Acting as elastically compressible means, rings or strips 34a by their addition to the exterior of elastomeric tube 34, result in a more constant force on friction shoes 32 of the shuttle device 38 against surface 16. This is because rings or strips 34a cause friction shoes 32 to lie closer to surface 16. Comparatively speaking, friction shoes 32 will experience a greater amount of friction with surface 16 than will O-rings 62, 64 against shuttle device 38 as that device slides thereover. This increased friction

between friction shoes 32 and surface 16 may be critical to start-up movement of the shuttle device 38.

Other embodiments of the invention will be apparent to those skilled in the art from consideration of the specification and practice of the invention disclosed herein.
5 It is intended that the specification and examples be considered as exemplary only, with a true scope and spirit of the invention being indicated by the following claims.

WHAT IS CLAIMED IS:

1. A fluid actuated friction damper comprising:
telescopically movable inner and outer bodies;
the outer body having an elongated, continuous
5 friction surface;

the inner body comprising friction shoe means
engageable with said continuous friction surface, fluid
pressure responsive means for exerting a normal force to urge
said friction shoe means against said continuous friction
10 surface, a shuttle device supporting said friction shoe means
for limited axial movement between end stops on said inner
body, and means for establishing fluid pressure communication
between an external source of pressurized fluid and said fluid
pressure responsive means when said shuttle device is at one
15 of said stops and for isolating said fluid pressure responsive
means from said external source when said shuttle device is
moved from said one stop.

2. The fluid actuated friction damper recited in
claim 1 comprising second friction shoe means and a second
20 fluid pressure responsive means for exerting a normal force
to urge said second shoe means against said continuous
friction surface independently of said first mentioned
friction shoe means, said first mentioned friction shoe means
and said second friction shoe means are urged against said
25 continuous friction surface under the same or different fluid
pressure.

3. The fluid actuated friction damper recited in
claim 2 wherein said friction surface comprises an interior
cylindrical surface and wherein each of said friction shoe
30 means comprises at least one arcuately convex segment
engageable with said interior cylindrical surface, said at
least one convex segment is provided with at least one venting
gap for air passage between said inner and outer bodies.

4. The fluid actuated friction damper recited in
35 claim 1 wherein said outer body includes a cylindrical wall
and an interior cylindrical surface to establish said
continuous friction surface, wherein said inner body includes

a rod extending axially from one end of said cylindrical wall, and further comprising guide bearings on opposite ends of said friction shoe means, said guide bearings maintaining concentric alignment of said inner and outer bodies independent of said friction shoe means, each comprising a plurality of spaced segments of low friction material.

5. The fluid actuated friction damper recited in claim 2 wherein said outer body includes a cylindrical wall and an interior cylindrical surface to establish said continuous friction surface, wherein said inner body includes a rod extending axially from an inner end within said cylindrical wall, through one end of said cylindrical wall to an outer end, and further comprising guide bearings for maintaining concentric alignment of said inner and outer bodies independent of said friction shoe means.

6. The fluid actuated friction damper recited in claim 5 comprising a fitting on the inner end of said inner body to support said second friction shoe means and said second fluid pressure responsive means, said friction shoe means extending axially beyond said second fluid responsive means to be supported directly by said fitting as a component of said guide bearings, said guide bearings and said friction shoe means each comprising a plurality of arcuate segments of low friction material wherein the segments of each of said guide bearings and friction shoe means are peripherally spaced by gaps.

7. The fluid actuated friction damper recited in claim 6 wherein said segments are formed of or substantially formed of: a material selected to develop interfacial friction by composite/counterface interface with surfaces in which they are in contact; a polytetrafluoroethylene filled polyphenylene sulfide; a ultra high molecular weight polyethylene; or a polytetrafluoroethylene and ultra high molecular weight polyethylene.

8. The fluid actuated friction damper recited in claim 1 wherein said outer body includes a cylindrical wall and an interior cylindrical surface to establish said continuous friction surface, wherein said means for establishing fluid pressure communication between an external

source of pressurized fluid and said fluid pressure responsive means comprises a hollow rod fixed to said inner body, said hollow rod extending axially from an inner end within said cylindrical wall, through one end of said cylindrical wall to an outer end, at least one radial port in said hollow rod located axially between said end stops, axially spaced slidable seal means between said hollow rod and said shuttle device to confine passage of fluid between said rod and said shuttle, and at least one shuttle port movable axially between one position located between said spaced seal means and another position located beyond the spaced seal means.

9. The fluid actuated friction damper recited in claim 2 wherein said means for establishing fluid pressure communication between an external source of pressurized fluid and said fluid pressure responsive means comprises a hollow rod fixed to said inner body, said hollow rod extending axially from an inner end with said cylindrical wall, through one end of said cylindrical wall to an outer end, said second fluid pressure responsive means being in continuous communication with the external source of pressure through said hollow rod.

10. The fluid actuated friction damper recited in claim 2 wherein said means for establishing fluid pressure communication between an external source of pressurized fluid and said fluid pressure responsive means comprises separate fluid passageways between the external source of pressurized fluid and said first mentioned fluid responsive means and between the external source of pressurized fluid and said second fluid responsive means, respectively, said fluid actuated friction damper comprising independently adjustable fluid pressure regulators in each of said separate fluid passageways.

11. A fluid actuated friction damper comprising:
telescopically movable inner and outer bodies,
each of said bodies having a continuous axial surface and a slide bearing to engage the continuous axial surface of the other of said bodies, thereby to maintain axial concentricity of the inner and outer bodies;

at least one of the inner and outer bodies

having a fluid pressure actuated friction shoe means in engagement with the continuous axial surface of the other of the inner and outer bodies under a normal force determined by regulated fluid pressure;

5 said slide bearing and said friction shoe means being of a material to provide a dry lubricant interface with the continuous axial surface contacted by the slide bearing and the friction shoe means, respectively.

12. The fluid actuated friction damper recited in
10 claim 11 comprising a combined slide bearing and friction shoe means on one of the bodies wherein the combined slide bearing and friction shoe means is defined by at least one axially extending arcuate shoe segment having a central portion and opposite end portions, said end portions bearing directly
15 between said inner and outer bodies and said central portion being forcible by fluid pressure to exert a variable normal friction force, wherein said material is substantially polytetrafluoroethylene filled polyphenylene sulfide, or substantially ultra high molecular weight polyethylene.

20 13. A fluid actuated friction damper comprising:
telescopically movable inner and outer bodies;
the outer body having inner and outer
cylindrical walls connected at opposite ends and separated
from each other between said opposite ends by an annular
25 space, said inner cylindrical wall defining an elongated, continuous friction surface;

the inner body having opposite ends and comprising friction shoe means engageable with said continuous friction surface, fluid pressure responsive means for exerting
30 a normal force to urge said friction shoe means against said continuous friction surface, and means for establishing fluid pressure communication between an external source of pressurized fluid and said fluid pressure responsive means, the opposite ends of the inner body and the opposite ends of
35 the outer body defining a pair of separated chambers with the inner cylindrical wall; and

a fluid passageway, including said annular space, for venting air between said separated chambers upon relative movement of said inner and outer bodies to inversely

vary the volume of said chambers, respectively.

14. The fluid actuated friction damper recited in claim 13 wherein said fluid passageway further includes ports opening through said inner cylindrical wall at opposite ends of said annular space and means for venting said annular space to the atmosphere.

FIG. 1

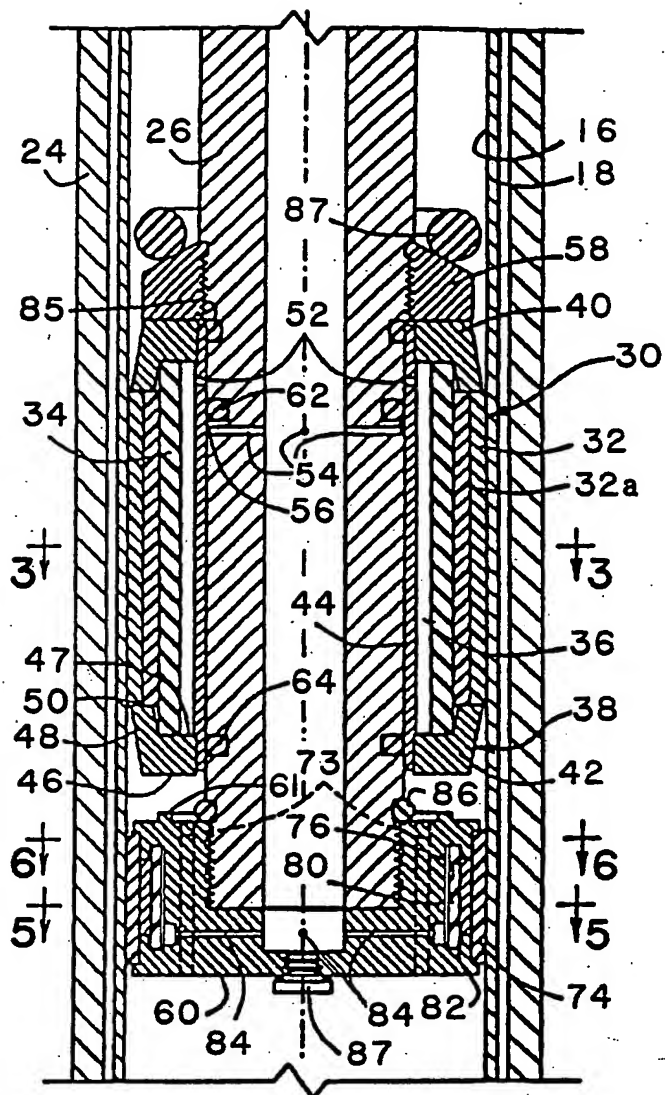
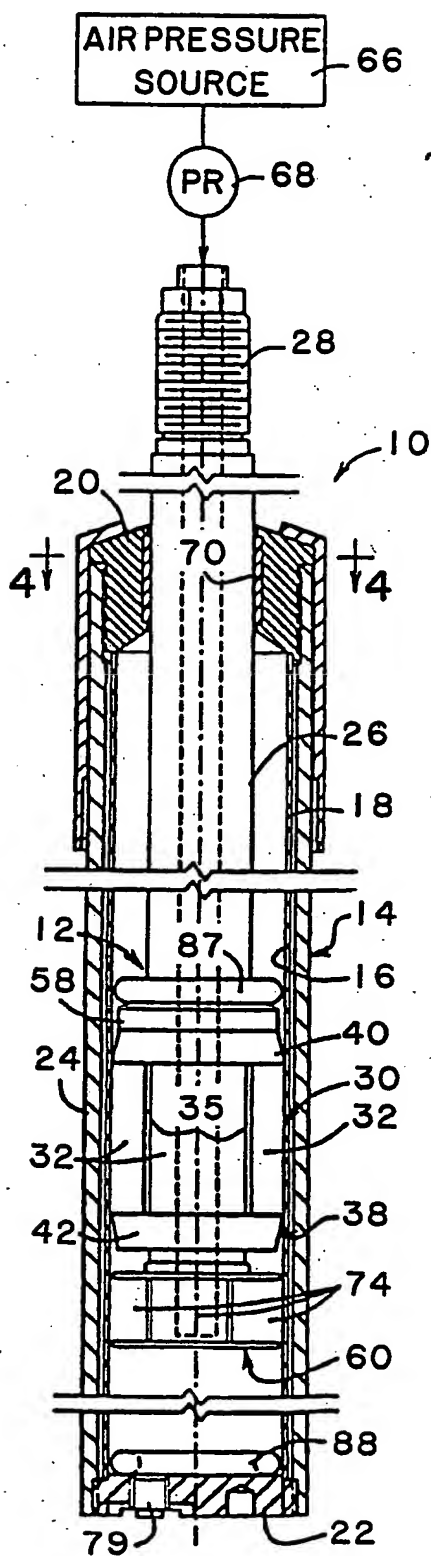


FIG. 2

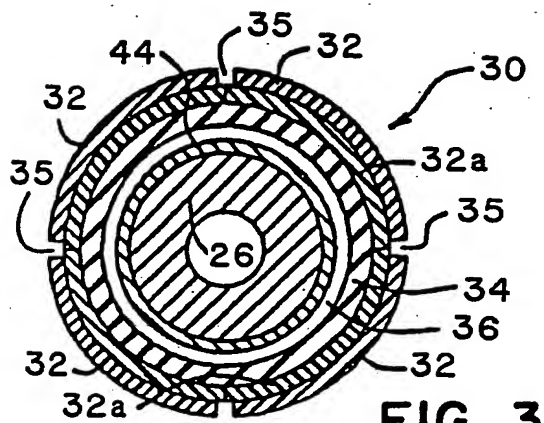


FIG. 3

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FIG. 4

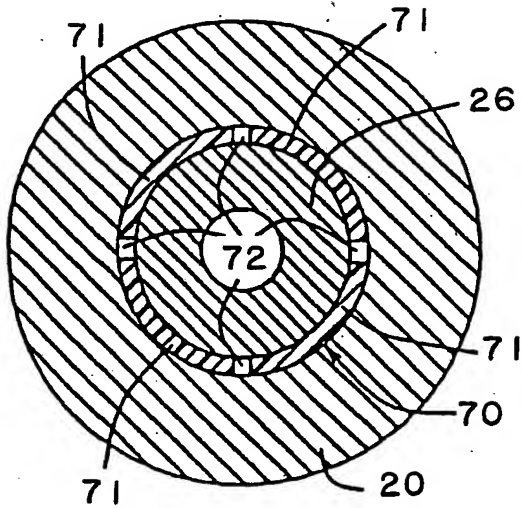


FIG. 5

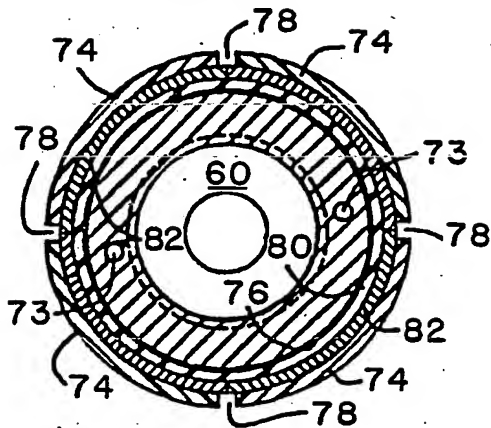


FIG. 6

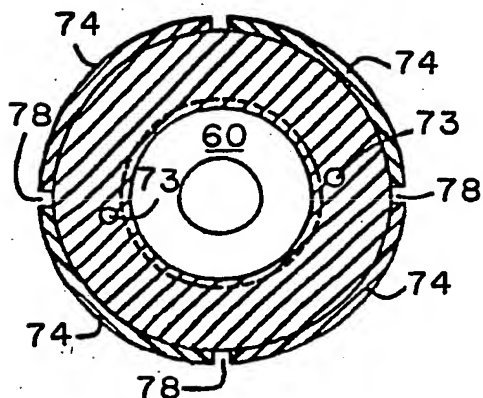
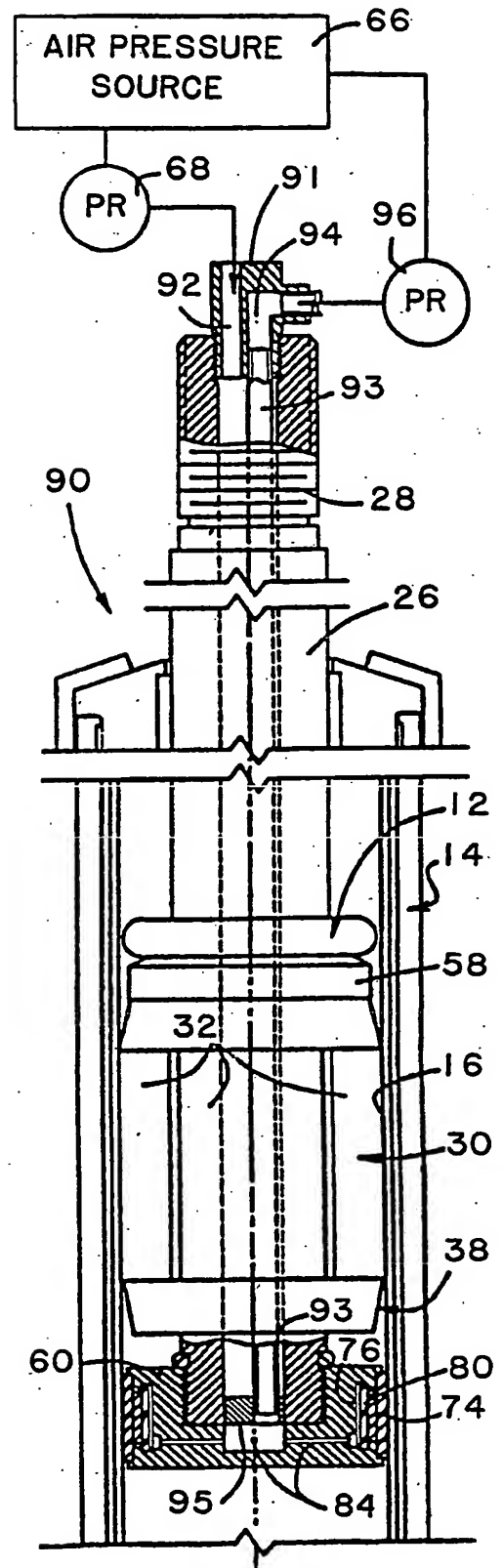


FIG. 7



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FIG. 8

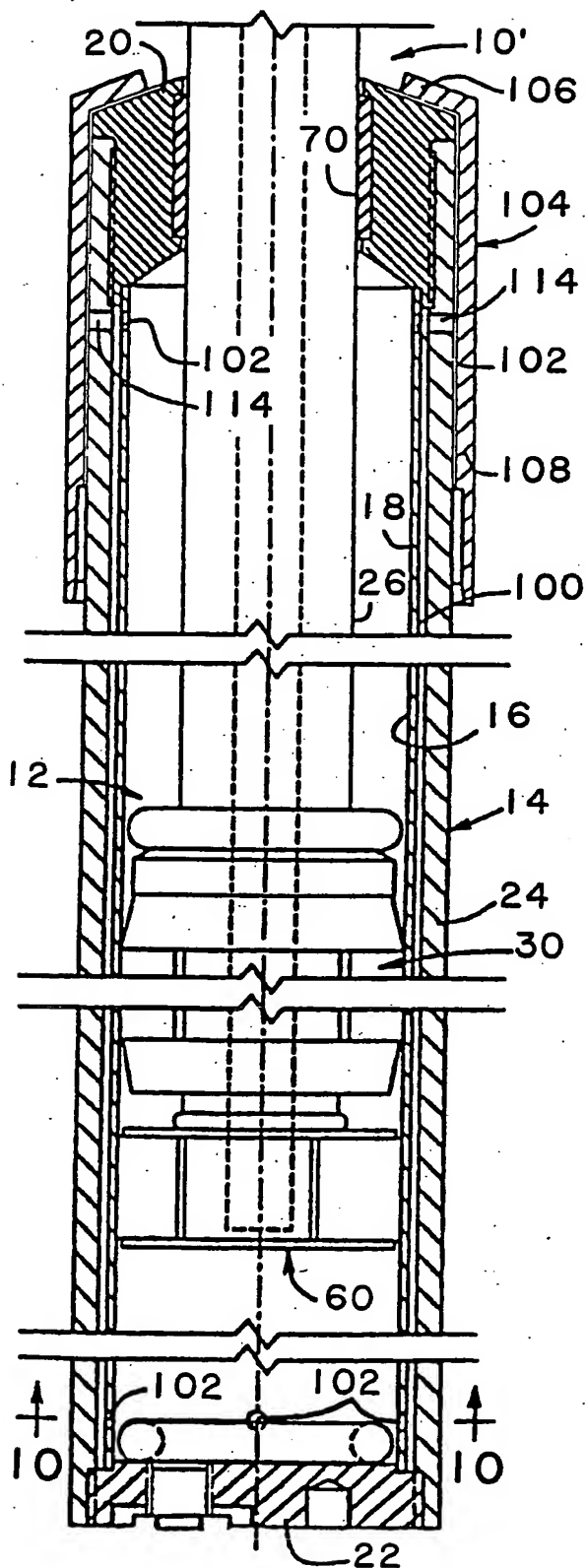


FIG. 9

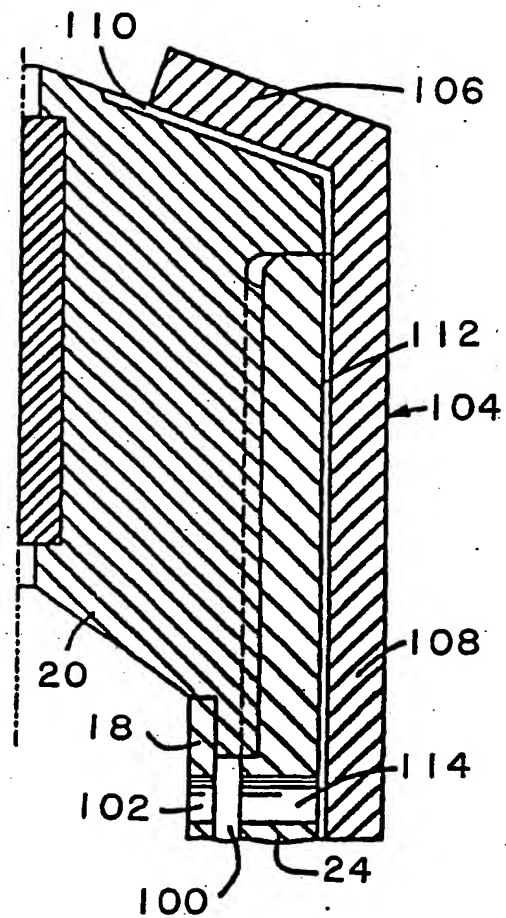


FIG. 10

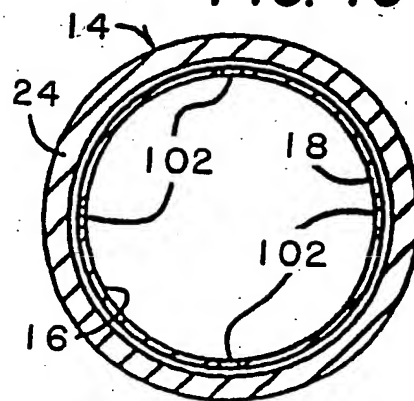


FIG. 13

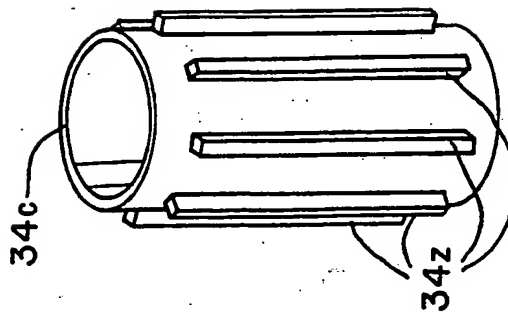


FIG. 12

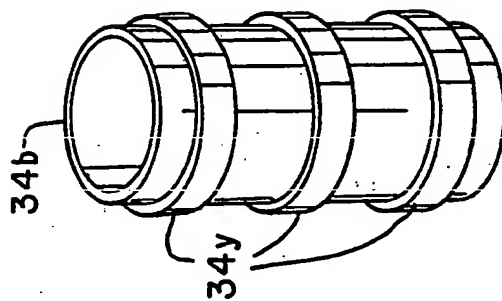
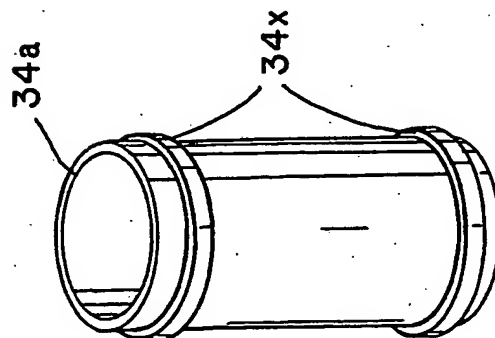


FIG. 11



INTERNATIONAL SEARCH REPORT

International application No.

PCT/US 94/01933

A. CLASSIFICATION OF SUBJECT MATTER
IPC 5 F16F11/00 F16F7/08

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 5 F16F

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A	EP,A,0 485 647 (PATON) 20 May 1992 see column 3, line 36 - column 5, line 23 see column 12, line 24 - line 54 see column 13, line 26 - line 29; claims 1-4; figures 1,4,6,7 -----	11 1,2,5,6, 9,10,13
A	GB,A,749 695 (DUNLOP RUBBER) 30 May 1956 see page 1, line 91 - page 2, line 108; figures 1,3 -----	1,11

☐ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

30 June 1994

Date of mailing of the international search report

22.07.94.

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Nordlund, J

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

P 94/01933

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP-A-0485647	20-05-92	US-A- 4979595	25-12-90
GB-A-749695		NONE	